

235 000
 11,8
 0,5
 20
 80
 -70-23,
 -70-23
 16.09.06.

machines to perform such operations, the product of the machines being free from wear iron contamination.

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 (, ,)
 « »
 16.09.06.

622.73

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 - ,

20 - (60 - 100)
 0,1 - 0,2
 110-
 (100 %)
 20 / .
) -

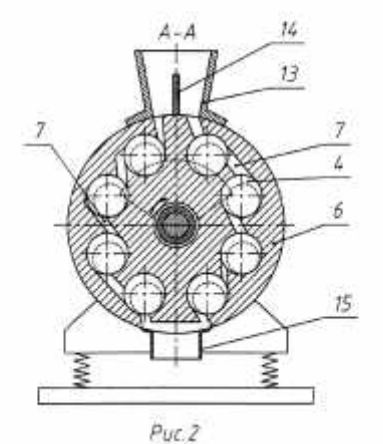
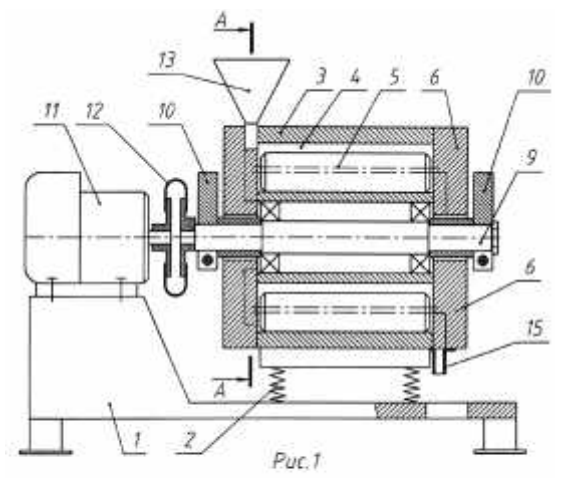
The process of coating fine 20 x (60-100) mcm cellulose microfbers with 0.1-0.2 mcm titanium dioxide powder by attrition in a 110-ML 8-cell vibrating mill charged with cylinder grinding medium has been investigated. A high (up to 100 %) surface area coverage and stable rutile adsorption by cellulose fibers has been recorded at capacity of 20 kg/h. Mechanical/chemical modification of powder surfaces (as by mechanical fusion, plating) is a fast growing market of demand in industrially developed countries. The actual demand of the market is now for a large scale commercial production of computer controlled

110-

.1 .2.

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7
7



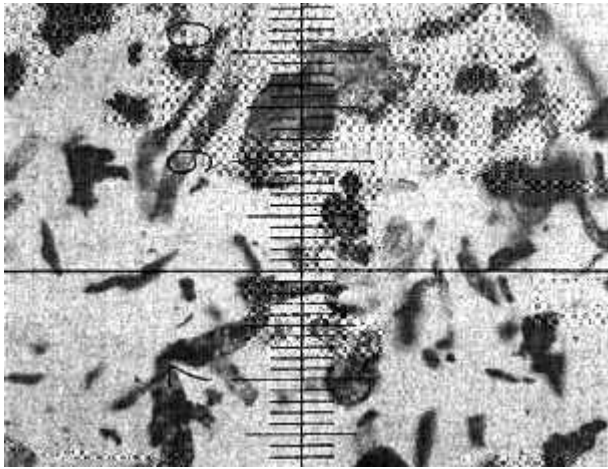
1 90% 5
10 / 4

Technical drawing of a roller mill (Fig. 1) showing a side view with numbered parts 1-13. It includes a motor (11), drive shaft (12), rollers (3, 4, 5, 6), and a hopper (13). The rollers are mounted on a frame (10) with bearings (9). The entire unit is supported by a base (1) with leveling legs (2).

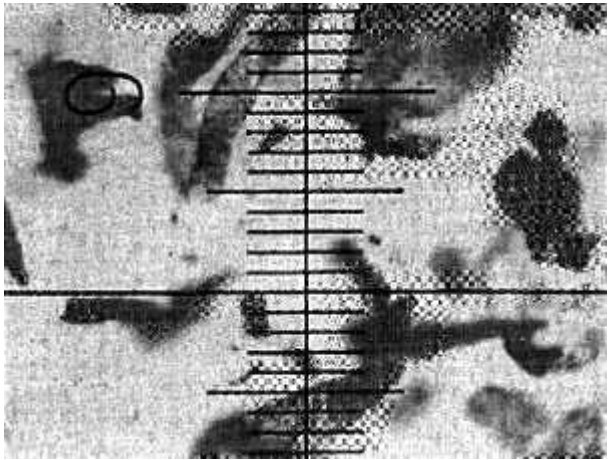
Technical drawing of a roller mill (Fig. 2) showing a top view of the roller assembly. It features a central shaft (14) with rollers (7) arranged around it. The rollers are supported by a frame (6) and bearings (4). The assembly is mounted on a base (15) with leveling legs. A hopper (13) is shown above the rollers.

1 90% 5
10 / 4

5-7) ()
0,1-0,2 60 10-20
100-200 50% 10; 25, 30
50:50%,
30:70; 25:75% 10:90%
n_c=1,518 100,
200 400 .
60 10-20
() - (30-150)
(1 2,
)
1
.2,



1. 50 : 50 %



1. 50 : 50 %

200 .

42 g (

8-12

2

21 g.

-
-
-

(48 36)

()

3424 . 45
35 4216 / 2,

60, 48 36
48 24

::

24 . 3.

(, ,)

1	2	3	4	5	6	7	8
1	50:50	- 45	25	3	4	98	
2	«	«	25	2	6	80-85	
3	«	48	25	2,5	12	85	
4	«	48 .24	25	2,5	12	90-95	
5	«	«	35	«	12	99,8	
6	«	«	35	«	13	95-97	
7	«	«	50		4	80-85	
8	«	.60 48 .24	25		6	85-90	
9	«	«	35		6	80	
10	«	«	35		8	78-80	
11	«	36 .24	25		4	90-95	
12	«	«	25		8	80-85	
13	«	36 .24	35		8	93-95	
14	25 : 75	36 .24	35		12	70	
15	«	48 .24	35		8	65-70	
16	25 : 75	48 .24	35		5,5	90-94	
17	«	.60+48+ 36 .24	35		20	50	
18	«	«	50		8	65	
19	«	.48 .24	25		6	68-70	
20	«	«	35		6	65-70	

1	2	3	4	5	6	7	8
22	50 : 50	.48, 24	35		4	98	
23	50 : 50 (W = 10%)	3 .48, 24	35		8	95	
24	50 : 50	«	35		8	65-70	
25	50 : 50	.48 .24	35		7	100	-
26	10 : 90		35		15	30	
27	39 : 70		35		15	80-85	

(25 50)

50

24 .

3 48 24 , . . .
3 90).

270 .

83.

10 %

25-30 % -15 / .

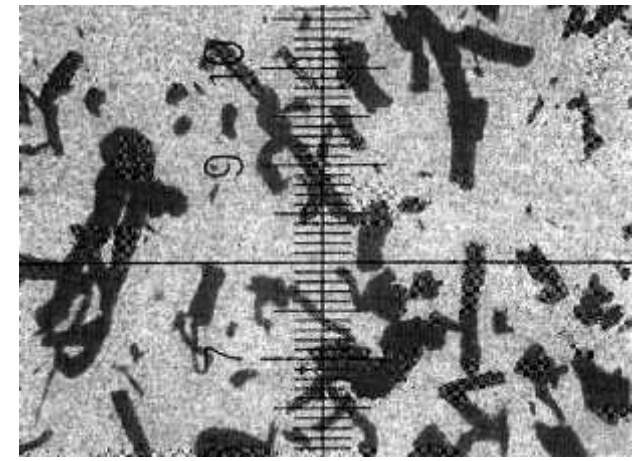
48 36

80-85 %
50:50 %

62

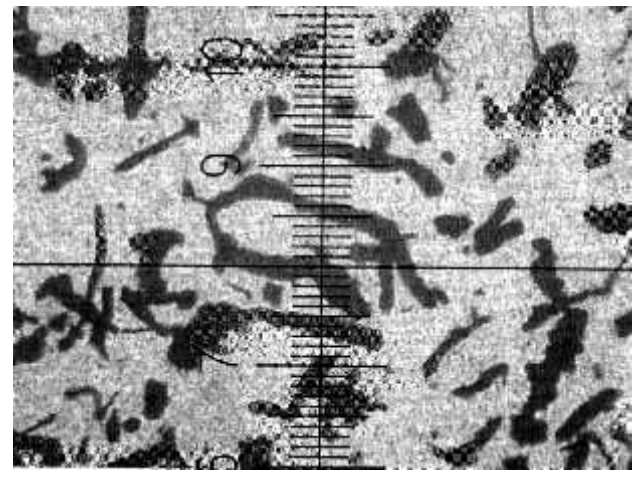
30 %, -

, 10 % -
 (,
),
 25-50 %
 -
 10 %
 (),
 (-
 -
 -
 -
 -
 :
 (30 - 150)
 5, 6,, 11, 13, 16, 22, 23, 25..
 50:50
 48 36
 35 , 4, 8 12 / . 24 ; -
 , 98 - 100 %.
 (



4. 22. 50 : 50 %.
 (98 %) 100 .

3 4).



3. 4. 50 : 50 %.
 (90 - 95 %).

, . . . ,
 110 -
 (. . .) 110-
 , 110-

(, , .).

5-10 / .

110-
0,14—0,8 / ³ 20 /

15-29 /

(, , .).

16.09.06.

666.26.342

· · , · · , · · , (,)

Experimental researches on studying influence of optimal grain compound of fused corundum, content of a matrix, molding-moisture content and frequency of vibrating formation on the properties of low-cement of concrete have been carried out. The results of optimization of the basic technological parameters of refractories from low-cement concrete are given.

[1 -4].

[5, 6].

6 ; 7 %

90 %, 0,1 .

· 6-3 - 28-38 % , · 3-1 - 28-40 % , · 1-0 - 27-40 % . 75 %

25 % , 2 .

4 . 7 % (, 100 %).

(40) 30 .

30 .

110⁰ 2 .

2409-95 , 4071.1-94. *

$$\dots = 3,10 \cdot x_1 + 3,06 \cdot x_2 + 3,09 \cdot x_3 - 0,089 \cdot x_1 \cdot x_2 (x_1 - x_2) + 0,135 \cdot x_1 \cdot x_3 \cdot (x_1 - x_3) + 0,427 \cdot x_2 \cdot x_3 (x_2 - x_3) - 0,022 \cdot x_1 \cdot x_2 (x_1 - x_2) - 2,529 \cdot x_1 \cdot x_3 \cdot (x_1 - x_3) - 0,112 \cdot x_2 \cdot x_3 (x_2 - x_3) - 0,585 \cdot x_1 \cdot x_2 \cdot x_3 / x^3; \quad (1)$$

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