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 : . - ∴ , 1989. - 56 . **2.**
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 , 1989. - . 2. - 177 . **3.** . ,
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 - 2002. - .325 - 332. **4.** . , . , . -
 , 1951. - 307c. **5.** . - ∴ ,
 1989. - 240c. **6.** . - ∴ , 1976. - 200 .

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533.9:546.11

• • , • • , • • ,

-

α
 $v'=v''=0,1,2,3)-$
 $\alpha (d^3 u, v' \rightarrow \sum_g^+, v'')$
 (-)

Evaluation of molecular hydrogen dissociation degree is made by measuring relation the ratio of the intensity of the line H_{α} of atomic hydrogen and the integral line intensity of the Fulcher α -system ($d^3 u, v' \rightarrow 3 \sum_g^+, v''; v'=v''=0,1,2,3$) in the low-pressure pulsed-periodic rf-discharge with an inhomogeneous distributions of the electric field. The obtained dissociation degree values characterize of the rf-power absorption region (skin-layer) in this discharge.

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α ($\lambda = 656,3$) [1, 2],

[3],

[4],

[5],

α [6] . . .

,

.

[7],

()

.

.

α

α ($d^3 u,$

$v' \rightarrow 3 \sum_g^+, v''; v'=v''=0,1,2,3$)-

()

$f = 0,833 \cdot 10^6$, , -63/0,44, -
 , 0,13 , . -
 150 600 , -
 , 7 160 -
 180 . 100 490 . -
 , 40 / 80 . -
 -
 60 , $\tau = 4,5 \cdot 10^{-3}$ -
 150 . , -
 , . -
 , , -
 , . -
 , z' -
 , φ -
 [8, 9]. -
 , 3 , -
 [10, 11], -
 . -
 . -
 3 ÷ 5 / . -
 , , -
 , , -
 , 2 , -
 , , -
 , -23 -
 1200 / . -

-84.

8-17,

-4

1

$$\alpha_2(d^3 u, v' \rightarrow \sum_g^+ v''; v' = v'' = 0,1,2,3) - [12].$$

$_2(d^3 u)$

:

$$e + H_2(X^1 \sum_g^+, \hat{n}) \rightarrow H_2(d^3 u, \hat{v}' < 4), \tag{1}$$

:

$$I_{H_2} = const \cdot n_e \cdot n_{H_2} \langle \dagger_{H_2} \cdot v_e \rangle, \tag{2}$$

$n_e \quad n_{H_2}^-$

, $\langle \dagger_{H_2} \cdot v_e \rangle -$

$_2(d^3 u)$

$_2(d^3 u),$

$_2(\sum_g^+)$ [13],

$_2(d^3 u)$

(1)

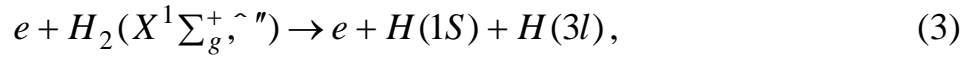
[14],

$_2(d^3 u)$

α

*(n = 3)

2:



α :

$$I_{H\alpha} = \text{const} (n_e \cdot n_{H_2} \langle \dagger_{H_2} \cdot v_e \rangle + n_e \cdot n_H \langle \dagger_{Hr} \cdot v_e \rangle), \quad (4)$$

$$\frac{n_H}{n_{H_2}} \frac{\langle \dagger_{Hr} \cdot v_e \rangle}{\langle \dagger_{H_2} \cdot v_e \rangle} = \frac{K_d}{1 - K_d} \cdot \frac{\langle \dagger_{Hr} \cdot v_e \rangle}{\langle \dagger_{H_2} \cdot v_e \rangle},$$

α .

* (n = 3) k_{ij} / k_{ji} , k_{ij}

k i.

(4) (2),

:

$$\frac{I_{Hr}}{I_{H_2}} = \frac{\langle \dagger_{Hr} \cdot v_e \rangle}{\langle \dagger_{H_2} \cdot v_e \rangle} + \frac{2K_d}{1 - K_d} \cdot \frac{\langle \dagger_{Hr} \cdot v_e \rangle}{\langle \dagger_{H_2} \cdot v_e \rangle}, \quad (5)$$

$$K_d = n_H / 2n_{H_2}^0 \quad , \quad n_{H_2}^0$$

2.

(1) (3) -

:

$$\langle \dagger \cdot v \rangle = \sqrt{\frac{2}{m}} \cdot \int_0^\infty \dagger(v) \cdot v \cdot f(v) \cdot dv, \quad (6)$$

m v - , $\dagger(v)$ - , $f(v)$ -

() . -

$$N, \quad = 0,707 \frac{E \cdot \epsilon}{(\epsilon^2 + \check{S}^2)^{\frac{1}{2}}} -$$

, S - , N - , \epsilon - .

[15].

[16],

$$n_e < 5 \cdot 10^{11} \text{ }^{-3}$$

, $n_e - (r)$.

- δ , $(= 15 \div 27) \quad \delta \approx 1$.

$\gg \lambda$, - ,

[17]:

$$= E^2(r) / \frac{dE^2(r)}{dr} , \quad (7)$$

$\lambda -$.

. [18] ,

400 d/ .

/N .

(r)

, ,

[19],

$$R = 0,8R \quad (R - \dots)$$

\overline{NR}

[20],

$$v''; v' = v'' = 0,1,2,3) \quad \alpha- \quad (d^3 u, v' \rightarrow \sum_g^+ = 1,6; 2,0; 5,0)$$

$\alpha-$

$$\overline{KR}, \quad [21]$$

$$\overline{KR} = \frac{\sqrt{\ln 2}}{4f\sqrt{f}} \cdot \frac{\Delta\}_{pq}^4}{c\Delta\}_{pq}} \cdot \frac{g_p}{q_q} \cdot A_{pq} \cdot n_q \cdot \dots \cdot R, \quad (8)$$

$$p \rightarrow q, \lambda_{pq} \dots ; g_i \dots ; \mu \dots$$

$$R = 1 \quad \overline{KR} \leq 1 \cdot 10^{-2} \quad n_q \leq 1 \cdot 10^{-3}, \dots \quad \Delta\}_{pq} = 0,02$$

$$*(n = 2), \quad 1 \cdot 10^{10} \quad ^{-3},$$

[21]

$$*(n = 2)$$

[21]:

$$n_e = 5 \cdot 10^{11} \quad ^{-3},$$

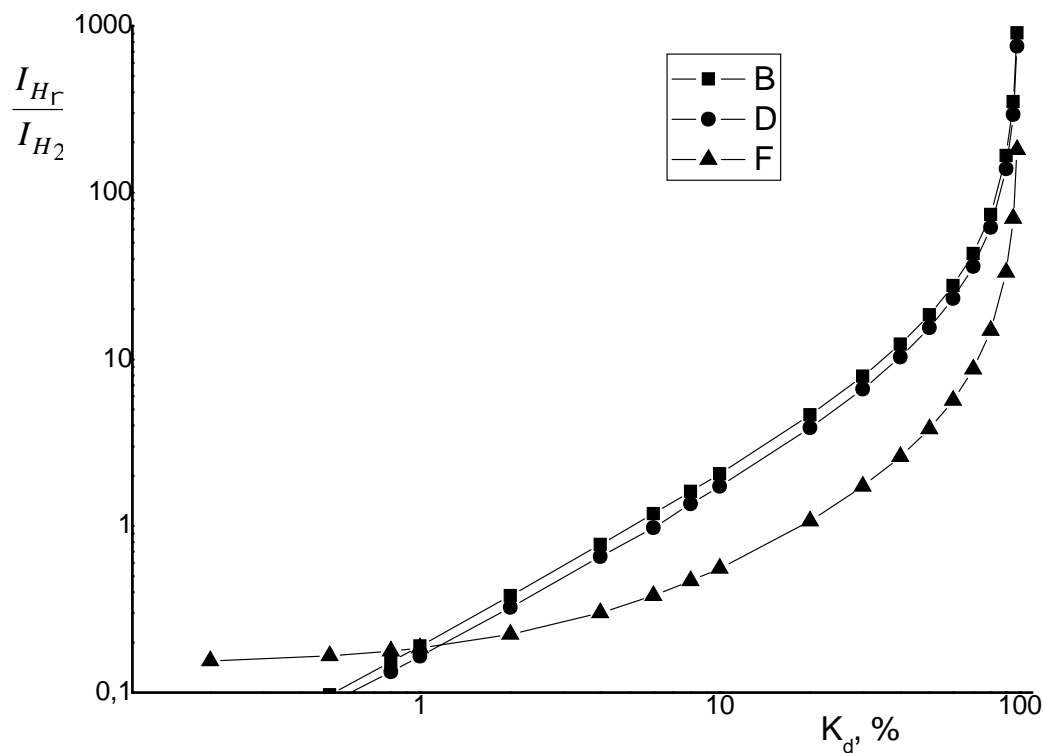
$$= 1,57$$

$$n_{H_2} = 9,8 \cdot 10^{13} \quad ^{-3} -$$

$$n_e \approx 5 \cdot 10^{12} \quad ^{-3} = 1,6 \div 2,0 \quad .$$

$$*(n=2) \quad 4,6 \cdot 10^7 \quad ^{-3},$$

$$n \quad *(n=2) \leq 1 \cdot 10^{10} \quad ^{-3}$$



$$-1,6 \quad , D-2,0 \quad , F-5,0 \quad .$$

80

$$= 15 \div 27$$

$$590 \div 640$$

[22].

$$\alpha \quad (d^3 u, v' \rightarrow \sum_g^+, v''; v' = v'' = 0).$$

$$= 1900 \div 2000 \text{ }^\circ \text{ .}$$

$$= 1,6 \div 2,0 \text{ .}$$

$$\bar{v} = \frac{3}{2} kT_e,$$

$$/N \text{ .}$$

$$/N$$

$$(1)$$

(3).

$$(45 \leq /N \leq 70$$

Td)

8 %, . . .

80

75 %.

(-)

: 1.

-2//

.-1984.- .10.-

3.-

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In the article the analysis of the state of question is conducted in the management by hard wastes. It is shown that complex processing of domestic wastes the most perspective decision of problems of rotation with wastes, foreseeing the use of innovations technologies of processing of raw materials components of HDW.